

Quantization of inductively shunted superconducting circuits

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We present a method for calculating the energy levels of superconducting circuits that contain highly anharmonic, inductively shunted modes with arbitrarily strong coupling. Our method starts by calculating the normal modes of the linearized circuit and proceeds with numerical diagonalization in this basis. As an example, we analyze the Hamiltonian of a fluxonium qubit inductively coupled to a readout resonator. While elementary, this simple example is nontrivial because it cannot be efficiently treated by the method known as “black-box quantization,” numerical diagonalization in the bare harmonic oscillator basis, or perturbation theory. Calculated spectra are compared to measured spectroscopy data, demonstrating excellent quantitative agreement between theory and experiment.

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I. INTRODUCTION

Superconducting qubits provide a promising platform for building a quantum computer, but experimental design requires highly accurate relationships between fabrication parameters and Hamiltonian parameters [1]. Successful approaches to this problem have involved finding effective superconducting circuit Hamiltonians with sufficient detail to accurately predict device behavior that are still simple enough for efficient diagonalization [2–12].

The method known as “black-box quantization,” in particular, decomposes a distributed microwave environment containing weakly anharmonic superconducting qubits into a few-body effective Hamiltonian [13]. It then numerically calculates the normal modes of the system in the limit that the Josephson junctions become linear inductors, writes the Hamiltonian in these normal coordinates, and truncates the Taylor expansions of the cosine terms. This method removes arbitrarily strong coupling terms, but with two caveats: (i) a finite Foster equivalent circuit, used to write a Hamiltonian from the normal modes, is not always accurate and (ii) truncating the cosine expansions is invalid for highly anharmonic qubits [Fig. 1(a)], by definition. The first issue has been resolved [14] using a Brune equivalent circuit [15]. In this paper, we propose and experimentally confirm a solution to the second issue.

Highly anharmonic qubits are prized for their *in situ* tunability and rich energy level structure, but the numerical diagonalization of their Hamiltonians is costly. A proper choice of basis for numerical diagonalization, which reflects the underlying physics of the system, is paramount to avoid disastrous convergence problems. For example, charge bases capture the band structure of capacitively shunted qubits like the Cooper pair box, while bound states in inductively shunted qubits like the fluxonium are conveniently described by harmonic oscillator bases [16]. Restricting our attention to the latter class, an early approach was to numerically diagonalize the full Hamiltonian, describing the qubit and the environment, in the bare harmonic oscillator basis [12]. An alternative method involves numerically diagonalizing the qubit Hamiltonian and treating its coupling to environmental normal modes perturbatively, which has limited applicability when this coupling is strong [17]. Our strategy is to use the

second quantized Fock basis for numerical diagonalization of the full Hamiltonian, after a transformation to the first quantized dressed mode basis. Our central result is that this method is advantageous when the coupling is sufficiently large.

This paper demonstrates the application of this strategy to a fluxonium qubit inductively coupled to a readout resonator (Sec. II), and it is organized as follows. In Sec. III, we linearize an effective electrical circuit of the system, transform into normal coordinates, and numerically diagonalize the Hamiltonian in this basis. Section IV examines the agreement between the calculated energy levels and experimental results.

II. PHYSICAL DEVICE

Experimentally, the fluxonium qubit is realized as one small Josephson junction in parallel with a series array of ~ 100 larger Josephson junctions [12]. In the limit of large size difference between these two types of junctions, the capacitances and nonlinear inductances across the array junctions may be neglected, and they form a collective, linear superinductance of up to ~ 300 nH [18]. If an external magnetic flux is threaded through this loop with magnitude $\Phi_{\text{ext}} = 0.5\Phi_0$ (with Φ_0 the magnetic flux quantum), the two lowest energy quantum states are approximately the symmetric and antisymmetric superpositions of countercirculating persistent-current states, similar to the flux qubit [5, 12]. This feature of the low-energy manifold motivates our use of inductive coupling as the link between the fluxonium qubit and readout resonator. This additional resonator is required for dispersive measurement and, in our system, is an LC oscillator whose capacitance and inductance are formed by an electric dipole antenna and another Josephson junction array, respectively. The inductive coupling is achieved by sharing junctions between the arrays of both oscillators. The resulting fluxonium-resonator system is depicted by the schematic diagram in Fig. 1(b).

To analyze this system, we (i) replace the distributed dipole antenna capacitance by a lumped element capacitor, and (ii) replace the large Josephson junction arrays by linear inductors. Approximation (i) is justified by the antenna length (~ 1 – 2 mm) being much smaller than the wavelength of the resonator (~ 3 – 6 cm) [19]. On the other hand, (ii) is permitted

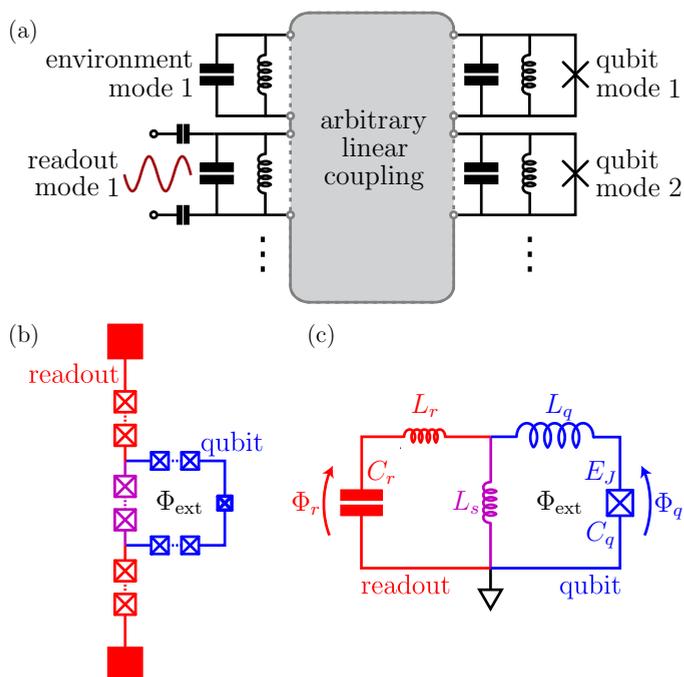


FIG. 1. (a) Schematic diagram of cQED systems involving a multimode microwave environment on the left and various highly anharmonic, inductively shunted qubits on the right. (b) Schematic diagram of the fluxonium-resonator system. The fluxonium qubit (blue) is threaded by an external magnetic flux Φ_{ext} and coupled to a dipole antenna used as a readout resonator (red) via an array of shared Josephson junctions (purple). (c) Circuit model of the system, obtained by replacing junction arrays with linear inductors.

when all array junctions are much larger than the small junction of the qubit and the relevant frequencies are below the fundamental mode of the array [18,20]. Figure 1(c) shows the resulting electrical circuit.

III. THEORY

A. Linearization

Having obtained a circuit with five elements, we may use Kirchoff's laws to write the Lagrangian in terms of two degrees of freedom: the flux across the capacitance of the readout resonator, Φ_r , and that across the small junction of the qubit, Φ_q . In the limit that $L_q \gg L_r \sim L_s$, i.e., the unshared inductance of the qubit is much larger than either the unshared inductance of the readout resonator or the shared inductance, the circuit is well described by the Lagrangian

$$\mathcal{L} = \frac{1}{2}C_r\dot{\Phi}_r^2 - \frac{1}{2(L_r + L_s)}\Phi_r^2 + \frac{L_s}{L_q(L_r + L_s)}\Phi_r\Phi_q + \frac{1}{2}C_q\dot{\Phi}_q^2 - \frac{1}{2L_q}\Phi_q^2 + E_J \cos(\varphi_q - \varphi_{\text{ext}}), \quad (1)$$

upon $\Phi_q \rightarrow \Phi_q - \Phi_{\text{ext}}$. Here, C_q and E_J denote the capacitance and Josephson tunneling energy of the small junction, while C_r represents the dipole capacitance of the readout mode. We have also introduced $\varphi_q \equiv 2\pi\Phi_q/\Phi_0$ as the difference in arguments of the superconducting order parameter on either side of the small junction. Analogously,

we have defined $\varphi_{\text{ext}} \equiv 2\pi\Phi_{\text{ext}}/\Phi_0$. Note that the first two terms in (1) describe the readout mode and the last three terms correspond to the qubit mode. All coupling between these modes is captured by the bilinear mutually inductive third term.

To linearize (1), we must temporarily dispense with components of the cosine term. For weakly anharmonic, capacitively shunted qubits, the cosine can be replaced by the quadratic term in its Taylor expansion [13]. An example is the transmon, which is a Josephson junction shunted by a large capacitance, and whose dynamics are governed by multiple Cooper pair tunneling events [11]. For highly anharmonic, inductively shunted qubits, the cosine should be discarded altogether. The fluxonium belongs to this class, owing to its large inductive shunt and single Cooper pair charging effects.

B. Normal modes

We decouple the linearized Lagrangian [$E_J \rightarrow 0$ in (1)] by diagonalizing the classical equations of motion. This amounts to changing variables to Φ_R and Φ_Q such that $\Phi_r = \lambda_1\Phi_R + \lambda_2\Phi_Q$ and $\Phi_q = \lambda_3\Phi_R + \lambda_4\Phi_Q$. The Lagrangian is now given by

$$\mathcal{L} = \frac{1}{2}C_R\dot{\Phi}_R^2 - \frac{1}{2L_R}\Phi_R^2 + \frac{1}{2}C_Q\dot{\Phi}_Q^2 - \frac{1}{2L_Q}\Phi_Q^2 + E_J \cos(\lambda_3\varphi_R + \lambda_4\varphi_Q - \varphi_{\text{ext}}), \quad (2)$$

where we have defined $\varphi_i \equiv 2\pi\Phi_i/\Phi_0$ to be the normal mode superconducting phases (with $i = R, Q$). Similarly, C_i and L_i denote the normal mode capacitances and inductances given by

$$C_R = \lambda_1^2 C_r + \lambda_3^2 C_q, \quad (3)$$

$$C_Q = \lambda_2^2 C_r + \lambda_4^2 C_q, \quad (4)$$

$$\frac{1}{L_R} = \frac{\lambda_1^2}{L_r + L_s} + \frac{\lambda_3^2}{L_q} - \frac{2\lambda_1\lambda_3 L_s}{L_q(L_r + L_s)}, \quad (5)$$

$$\frac{1}{L_Q} = \frac{\lambda_2^2}{L_r + L_s} + \frac{\lambda_4^2}{L_q} - \frac{2\lambda_2\lambda_4 L_s}{L_q(L_r + L_s)}. \quad (6)$$

We note that this normal mode basis, in which the coupling between modes is entirely captured by the cosine term in (2), conveniently makes obvious the inherited nonlinearity of the readout as well as the nonlinear nature of the coupling [13]. To draw an analogy to the circuit quantum electrodynamics (cQED) literature, we observe that $|\lambda_1| \gg |\lambda_2|$ and $|\lambda_3| \ll |\lambda_4|$ in our devices (see Table II), which means that mode R is vastly more linear than mode Q [21]. This allows us to refer to modes R and Q in (2) as the *readoutlike* and *qubitlike* modes, respectively, which we will henceforth refer to as *readout* and *qubit*.

We then apply a Legendre transform and define the conjugate charges $Q_i \equiv \partial\mathcal{L}/\partial\Phi_i$ for the two normal modes [3]. These steps permit the writing of the quantum Hamiltonian

$$\hat{H} = \frac{1}{2C_R}\hat{Q}_R^2 + \frac{1}{2L_R}\hat{\Phi}_R^2 + \frac{1}{2C_Q}\hat{Q}_Q^2 + \frac{1}{2L_Q}\hat{\Phi}_Q^2 - E_J \cos(\lambda_3\hat{\varphi}_R + \lambda_4\hat{\varphi}_Q - \varphi_{\text{ext}}). \quad (7)$$

C. Numerical diagonalization

We express this Hamiltonian in the normal mode harmonic oscillator basis $\{|nm\rangle\}$, where n and m correspond to the number of excitations in the readout and qubit modes, which yields the (infinite-dimensional) matrix

$$\hat{H} = \hbar \sum_{n,m \in \mathbb{N}} (\omega_R n + \omega_Q m) |nm\rangle \langle nm| - E_J \sum_{n,n',m,m' \in \mathbb{N}} [\cos \varphi_{\text{ext}} (c_{nn'}^R c_{mm'}^Q + s_{nn'}^R s_{mm'}^Q) + \sin \varphi_{\text{ext}} (c_{nn'}^R s_{mm'}^Q - s_{nn'}^R c_{mm'}^Q)] |nm\rangle \langle n'm'|. \quad (8)$$

Here, ω_i is the dressed harmonic oscillator frequency of normal mode i . The cosine and sine matrix elements can be computed analytically as follows, where \mathcal{L}_a^b are the associated Laguerre polynomials and it is understood that $\lambda_R = \lambda_3$ and $\lambda_Q = \lambda_4$ [22].

$$c_{k\ell}^i \equiv \langle k | \cos(\lambda_i \hat{\varphi}_i) | \ell \rangle = \begin{cases} (-1)^{(\ell-k)/2} \sqrt{\frac{k!}{\ell!}} (\lambda_i \varphi_i^{\text{ZPF}})^{\ell-k} e^{-(\lambda_i \varphi_i^{\text{ZPF}})^2/2} \mathcal{L}_k^{\ell-k} [(\lambda_i \varphi_i^{\text{ZPF}})^2] & (k + \ell \text{ even}, k \leq \ell) \\ 0 & (k + \ell \text{ odd}), \end{cases} \quad (9)$$

$$s_{k\ell}^i \equiv \langle k | \sin(\lambda_i \hat{\varphi}_i) | \ell \rangle = \begin{cases} 0 & (k + \ell \text{ even}) \\ (-1)^{(\ell-k+1)/2} \sqrt{\frac{k!}{\ell!}} (\lambda_i \varphi_i^{\text{ZPF}})^{\ell-k} e^{-(\lambda_i \varphi_i^{\text{ZPF}})^2/2} \mathcal{L}_k^{\ell-k} [(\lambda_i \varphi_i^{\text{ZPF}})^2] & (k + \ell \text{ odd}, k \leq \ell). \end{cases} \quad (10)$$

We treat the full analytic expression (8)–(10) for the Hamiltonian matrix of the fluxonium-resonator system as in Fig. 1(c) (when $L_q \gg L_r \sim L_s$). Computing the lowest energy levels requires truncating both readout and qubit Hilbert spaces. This is done by restricting the basis to $\{|nm\rangle : n \leq n_0, m \leq m_0\}$ with finite cutoff dimensions n_0 and m_0 . We choose $n_0 \sim 5$ and $m_0 \sim 20$ in order to simultaneously minimize truncation errors and computational cost [23]. Such numerical diagonalization yields the full solution to the time-independent Schrödinger equation

$$\hat{H} |n\mu\rangle = E_{n\mu} |n\mu\rangle, \quad (11)$$

where μ denotes the qubit excitation. The computed energy spectrum for device A (see Table I) as a function of threaded external magnetic flux Φ_{ext} is plotted in Fig. 2(a) for the first nine transitions of the system from its ground state.

In order to assign the quantum numbers n and μ to these energy levels, which undergo anticrossings as external flux is varied as in Fig. 2, we additionally diagonalize a decoupled version of the Hamiltonian (7), \hat{H}_0 . This Hamiltonian is obtained by setting $\hat{\varphi}_R \rightarrow 0$ in the argument of the cosine in (7) or by setting $c_{nn'}^R \rightarrow 1$ and $s_{nn'}^R \rightarrow 0$ in (8). Computing the energy levels for \hat{H}_0 only requires truncating the qubit Hilbert space. This time, the basis is restricted to $\{|nm\rangle : m \leq m_0\}$ with finite m_0 . As before, we take $m_0 \sim 20$, and we reiterate that numerical methods are the only tractable option. This procedure results in the solution of

$$\hat{H}_0 |n\mu\rangle_0 = \epsilon_{n\mu} |n\mu\rangle_0. \quad (12)$$

TABLE I. Parameters used for energy level calculations in Figs. 2 and 3.

	Device A	Device B
C_r	20.3 fF	20.1 fF
L_r	15.6 nH	19.7 nH
C_q	5.3 fF	5.9 fF
L_q	386 nH	430 nH
E_J	6.20 GHz	9.08 GHz
L_s	4.5 nH	2.9 nH

Note that the eigenstates are easily separable; that is, $|n\mu\rangle_0 = |n\rangle |\mu\rangle_0$ and $\epsilon_{n\mu} = \hbar\omega_R n + \epsilon_\mu$. In other words, the decoupled spectrum has built-in quantum numbers. Quantum numbers are then assigned by comparing the coupled energy spectrum $E_{n\mu}$ to the decoupled spectrum $\epsilon_{n\mu}$. In the limit of weak coupling, we may simply take n and μ for a given coupled level to be those of the nearest decoupled level. In this scheme, the quantum numbers labeling a chosen energy level abruptly switch at level anticrossings, as shown in Fig. 2(b).

D. Comparison with other methods

To benchmark our method, we contrast the essential steps with those of Refs. [12,13,17]. Respectively, the central differences are transforming to normal coordinates, truncating the cosine term, and using perturbation theory for the qubit-environment coupling.

1. Normal modes

Numerical diagonalization of the Hamiltonian corresponding to (1) in the bare harmonic oscillator basis $\{\Phi_r, \Phi_q\}$ was carried out in the case of capacitive coupling in Ref. [12]. Our approach performs this diagonalization in the dressed harmonic oscillator basis $\{\Phi_R, \Phi_Q\}$. This transformation allows for more aggressive Hilbert space truncation when numerically diagonalizing, provided the residual coupling mediated by the cosine is smaller than the initial linear coupling:

$$\frac{L_s}{L_r + L_s} < \frac{|\lambda_3|}{\lambda_4}. \quad (13)$$

The left-hand side in the above inequality represents the turns ratio between the shared inductance and the readout inductance, while the right-hand side represents the degree of mode hybridization. Criterion (13) is satisfied for a broad class of systems, including our physical devices (see Tables I and II).

2. Cosine truncation

In Ref. [13], the cosine term in (7) is Taylor expanded and the first few terms are retained. In our treatment, no truncation

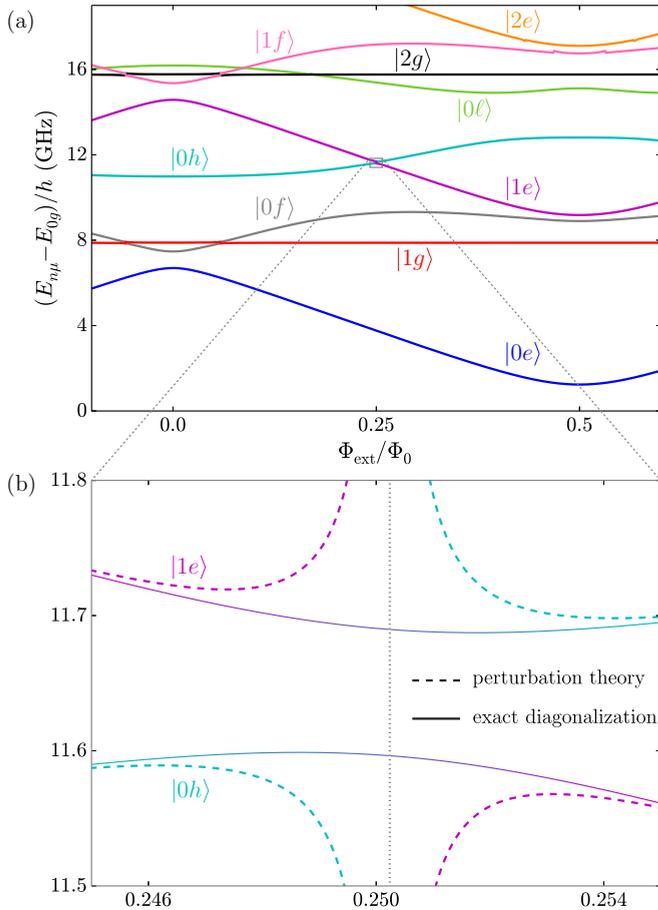


FIG. 2. (a) Energy levels $E_{n\mu}$ of the fluxonium-resonator system as a function of external flux Φ_{ext} . The zero-point energy is taken to be E_{0g} and energies are given in frequency units, while flux is given in multiples of the magnetic flux quantum Φ_0 . (b) Anticrossing between the $0 \rightarrow 1$ readout transition and the $e \rightarrow h$ qubit transition, and the divergence of second-order perturbation theory.

is employed. This truncation makes it extremely easy to calculate the off-diagonal Hamiltonian matrix elements, facilitating numerical diagonalization or perturbative analysis. For either mode, this step requires that (i) a well-defined classical steady state $\langle \varphi_i \rangle$ is found and (ii) the quantum fluctuations of the phase φ_i^{ZPF} are small. Condition (i) guarantees that the Taylor expansion is possible, and we note that it is patently violated for the fluxonium qubit, since there are multiple potential minima. Condition (ii) ensures that the expansion converges rapidly,

TABLE II. Normal mode coefficients corresponding to parameter sets in Table I.

	Device A	Device B
$1 - \lambda_1$	1.5×10^{-3}	4.1×10^{-4}
λ_2	1.5×10^{-2}	8.4×10^{-3}
λ_3	-5.6×10^{-2}	-2.9×10^{-2}
$1 - \lambda_4$	1.1×10^{-4}	3.5×10^{-5}

and it mathematically amounts to

$$Z_i = \sqrt{\frac{L_i}{C_i}} \ll R_Q = \frac{\hbar}{(2e)^2}, \quad (14)$$

where Z_i is the characteristic impedance of mode i and R_Q is the impedance quantum. This highlights the fact that truncating the cosine expansion is permissible only for low impedance modes.

3. Perturbation theory

Independently of the considerations in the previous two sections, the qubit-readout coupling terms may be treated perturbatively, as in Ref. [17]. This treatment greatly reduces the Hilbert space size for numerical diagonalization, at the expense of additional calculations of perturbed eigenstates and energy levels. For a variety of systems, perturbative expansions do not converge quickly enough to provide an advantage in computational complexity over numerical diagonalization [see Fig. 2(b) as well as Appendix A for an application to our system]. Simply stated, perturbation theory is not efficient for systems with sufficiently large qubit-environment coupling.

IV. AGREEMENT WITH EXPERIMENT

We test the accuracy of our circuit model and analysis by comparing the simulated spectrum to experimentally obtained spectroscopy data at various values of Φ_{ext} and for two devices with different parameters (Table I).

These devices were measured in an impedance-matched, copper rectangular waveguide mounted in a dilution refrigerator at ~ 20 mK. Two-tone microwave pulses were incident on the device and then demodulated at 300 K using a heterodyne interferometry setup (Appendix B) [9]. This allowed for the measurement of the readout $0 \rightarrow 1$ transition frequency, the qubit $g \rightarrow e$ transition frequency, and the dispersive shift χ of the readout by the qubit. Data is shown in Fig. 3.

It is clear that the measured readout $0 \rightarrow 1$ transition frequency and the qubit $g \rightarrow e$ transition frequency should be compared to the quantities $(E_{1g} - E_{0g})/h$ and $(E_{0e} - E_{0g})/h$ obtained from diagonalization, respectively, in the limit of zero temperature. The dispersive shift χ may also be computed from diagonalization via

$$\chi \equiv \frac{1}{h} [(E_{1e} - E_{0e}) - (E_{1g} - E_{0g})]. \quad (15)$$

These three numerically computed quantities are also plotted in Fig. 3. In addition, the dispersive shift calculated from the perturbative approach in Appendix A is also plotted in Figs. 3(e) and 3(f).

The parameters in Table I are found by fitting these simulated quantities to those measured experimentally. The readout capacitance C_r is predicted independently using a commercial high-frequency electromagnetic solver (Ansys HFSS), a finite-element electromagnetic modeling program. The chief discriminating factor between device A and device B is the qubit-readout coupling strength. The turns ratio between the shared inductance and the readout unshared inductance is $L_s/L_r \approx 0.29$ for device A, while $L_s/L_r \approx 0.15$ for device B. Moreover, the value of E_J is roughly 50% higher for device

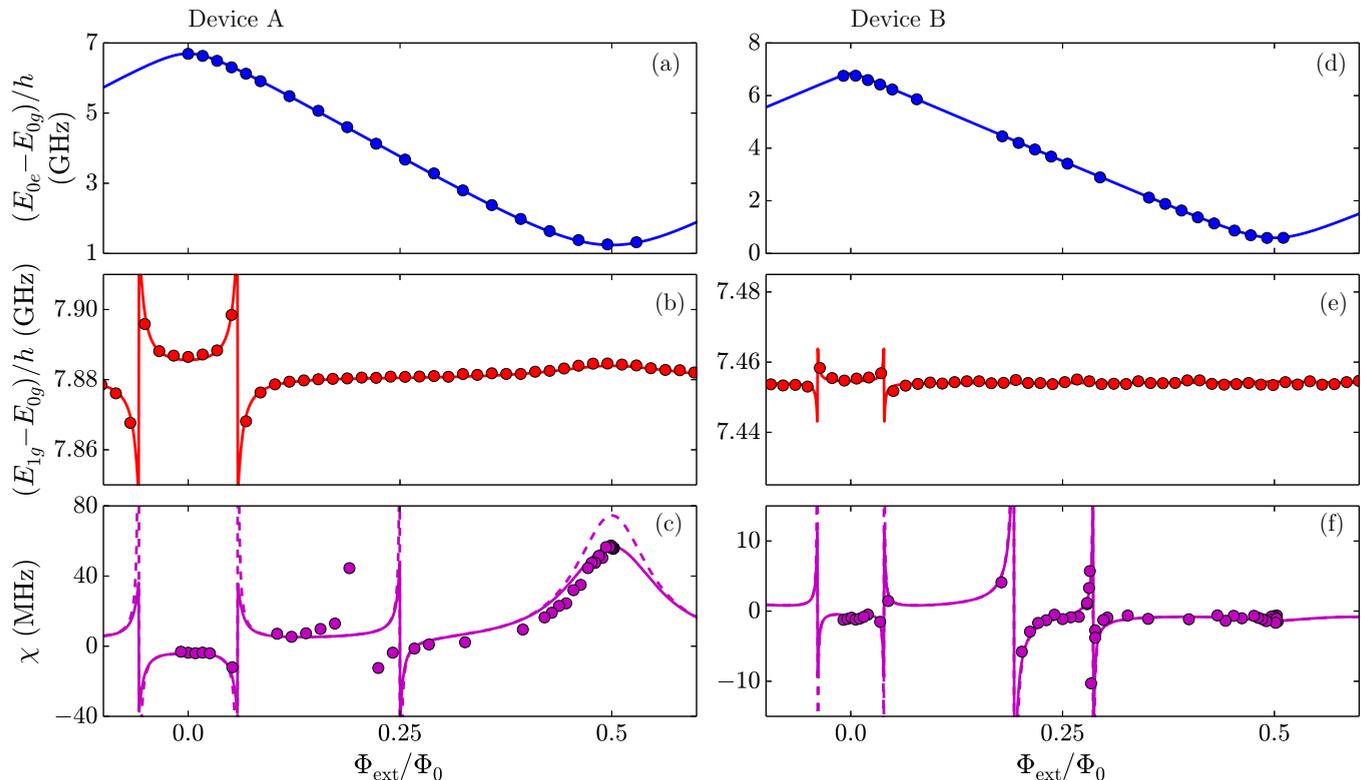


FIG. 3. (a), (b) Blue: qubit $g \rightarrow e$ transition frequency. (c), (d) Red: readout $0 \rightarrow 1$ transition frequency. (e), (f) Purple: dispersive shift χ . All results are plotted as a function of external flux Φ_{ext} in units of Φ_0 . Circles indicate data taken using two-tone spectroscopy (blue), single-tone spectroscopy (red), and single-tone spectroscopy preceded by qubit state preparation (purple). Solid lines indicate theoretical fits obtained from numerical diagonalization. Dashed lines indicate results from second-order perturbation theory.

B than device A, resulting in a significantly lower $g \rightarrow e$ transition frequency at $\Phi_{\text{ext}} = 0.5\Phi_0$.

Theoretical and experimental results in Fig. 3 agree well, with the exception of two features. First, the location in external flux of the singularity in χ for device A differs between the model and measurements. We attribute this to the $e \rightarrow h$ qubit transition crossing the $0 \rightarrow 1$ readout transition [see Fig. 2(b)], which involves the $|0h\rangle$ state, whose transition frequency is ~ 12 GHz from the ground state. Our approximation of the Josephson junction array composing the unshared superinductance of the qubit breaks down at these frequencies due to the fundamental mode of the array occurring at ~ 11 GHz [18,20,24]. Second, perturbation theory consistently overestimates the dispersive shift in the vicinity of avoided crossings for both device A and (to a lesser extent) device B. This is most apparent at $\Phi_{\text{ext}} = 0.5\Phi_0$ for device A, at which point χ is calculated to be 75 MHz using perturbation theory and 57 MHz using numerical diagonalization. The error in the perturbative calculation stems from the $e \rightarrow f$ qubit transition becoming nearly resonant with the $0 \rightarrow 1$ readout transition [see Fig. 2(a)].

The strong variation of the energy spectrum with external flux is apparent in Fig. 2(a) [25]. This indicates a valuable feature of the fluxonium-resonator system: the qubit, readout, and qubit-readout coupling all behave differently as Φ_{ext} is swept. As an additional example, the inherited nonlinearity of the readout resonator, extracted from the computed energy spectrum, can undergo strong variation with both qubit state

and Φ_{ext} (Appendix C). This allows access to multiple coupling regimes and cQED Hamiltonians within a single device.

V. CONCLUSION

We have constructed an effective circuit [Fig. 1(c)] and Hamiltonian (7) for the fluxonium-resonator system: a device consisting of a readout resonator and fluxonium qubit, where all inductances are formed by arrays of Josephson junctions and the readout-qubit coupling is realized by a partially shared inductance. The low-energy spectrum of this device has been computed using a new method: numerical diagonalization in the dressed mode basis. Quantitative agreement with experimental results was obtained for nearly all values of Φ_{ext} . This demonstrates the utility of our method and we expect it to be applicable in diagonalizing a broad class of superconducting circuit Hamiltonians, such as strongly coupled fluxonium qubits, inductively shunted transmon qubits, and fluxonium qubits coupled to readout resonators via shared flux qubits.

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APPENDIX A: PERTURBATION THEORY

To treat the qubit-readout coupling in (7) perturbatively, as shown in Fig. 2(b) and mentioned in Sec. IV, we Taylor expand the cosine term about $\lambda_3 = 0$, because $|\lambda_3| \ll 1$. Discarding the $O(\lambda_3^3)$ terms results in

$$\begin{aligned} \hat{H} = & \frac{1}{2C_R} \hat{Q}_R^2 + \frac{1}{2L_R} \hat{\Phi}_R^2 + \frac{1}{2C_Q} \hat{Q}_Q^2 + \frac{1}{2L_Q} \hat{\Phi}_Q^2 \\ & - E_J \left[\cos(\lambda_4 \hat{\Phi}_Q - \varphi_{\text{ext}}) - \lambda_3 \hat{\Phi}_R \sin(\lambda_4 \hat{\Phi}_Q - \varphi_{\text{ext}}) \right. \\ & \left. - \frac{1}{2} (\lambda_3 \hat{\Phi}_R)^2 \cos(\lambda_4 \hat{\Phi}_Q - \varphi_{\text{ext}}) \right]. \end{aligned} \quad (\text{A1})$$

Although the same assumption ($|\lambda_3| \ll 1$) justifies both the replacement of (7) by (A1) and the use of perturbation theory on the last two terms in (A1), the majority of error arises from the latter step. We may then consider the first five terms in (A1) as the unperturbed Hamiltonian \hat{H}_0 , which coincides with the decoupled Hamiltonian from Sec. III C. First- and second-order perturbation theory may then be used on the seventh and sixth terms in (A1), respectively. This results in corrections of the form

$$\begin{aligned} \delta\epsilon_{n\mu} = & E_J (\lambda_3 \varphi_R^{\text{ZPF}})^2 \left(n + \frac{1}{2} \right) {}_0\langle \mu | \cos(\hat{\Phi}_Q - \varphi_{\text{ext}}) | \mu \rangle_0 \\ & + E_J^2 (\lambda_3 \varphi_R^{\text{ZPF}})^2 \sum_{\mu' \neq \mu} \frac{(2n+1)(\epsilon_\mu - \epsilon_{\mu'}) + \hbar\omega_R}{(\epsilon_\mu - \epsilon_{\mu'})^2 - (\hbar\omega_R)^2} \\ & \times {}_0\langle \mu' | \sin(\hat{\Phi}_Q - \varphi_{\text{ext}}) | \mu \rangle_0^2, \end{aligned} \quad (\text{A2})$$

completing the calculation of the energy levels $\epsilon_{n\mu} + \delta\epsilon_{n\mu}$ for the system via perturbative treatment of the readout-qubit coupling.

APPENDIX B: EXPERIMENTAL DETAILS

The two devices in Sec. IV were fabricated with aluminum on sapphire substrates using double-angle evaporation. In particular, bridge-free fabrication was used for the Josephson junctions [26]. The rectangular waveguide enclosing the resulting devices had 0.3 dB insertion loss across frequencies in the passband of 6.5–9 GHz. An applied external magnetic flux was threaded through the qubit [Figs. 1(b) and 1(c)] by passing a current through a superconducting coil around the midsection of the waveguide. Thermally anchored to the mixing chamber of a dilution refrigerator, this sample holder was magnetically isolated from its environment using high-permeability metallic and aluminum shields.

Input microwave signals were channeled into the waveguide through 63 dB of attenuation as well as infrared-frequency filters [27,28]. Output signals were passed through two isolators and then amplified using a high-electron-mobility transistor and a commercial microwave amplifier at 300 K. Single-tone spectroscopy using a vector network analyzer was used to determine the readout $0 \rightarrow 1$ transition frequency. We used two-tone spectroscopy to measure the qubit $g \rightarrow e$ transition

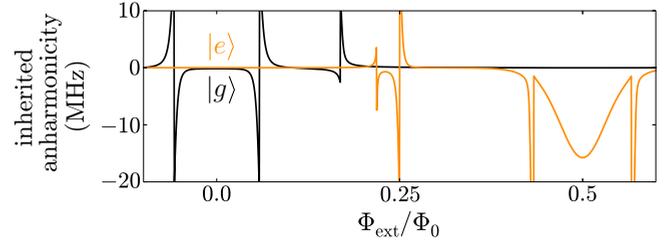


FIG. 4. Inherited anharmonicity of the readout resonator as a function of external flux Φ_{ext} , defined as the difference between the $1 \rightarrow 2$ and $0 \rightarrow 1$ readout transition frequencies. Results from numerical diagonalization are shown for the qubit in state $|g\rangle$ (black) and state $|e\rangle$ (orange).

frequency. This involved sending a $\sim 100 \mu\text{s}$ saturation pulse at a variable qubit frequency followed by a $\sim 30 \mu\text{s}$ readout pulse at the fixed $0 \rightarrow 1$ transition frequency. Our room temperature heterodyne interferometry setup independently mixed the outgoing readout pulse as well as a reference readout pulse with local oscillator signals (at a frequency detuned from the readout by 50 MHz) and then digitized and analyzed the 50 MHz components. Finally, the dispersive shift χ was measured by applying a π -rotation pulse at the qubit $g \rightarrow e$ transition frequency and then performing pulsed single-tone spectroscopy of the $0 \rightarrow 1$ readout transition with the heterodyne interferometry setup. This was compared to the result from the same procedure with an off-resonant π pulse to determine χ .

APPENDIX C: INHERITED ANHARMONICITY OF THE READOUT

Further proof of the tunability of the fluxonium-resonator system as a function of Φ_{ext} is demonstrated in Fig. 4. The calculated qubit state-dependent inherited anharmonicity of the readout is shown as a function of external flux for device A. We define this inherited anharmonicity as

$$\frac{1}{\hbar} [(E_{2\mu} - E_{1\mu}) - (E_{1\mu} - E_{0\mu})], \quad (\text{C1})$$

that is, analogously to the self-Kerr effect [29,30]. Remarkably, this inherited anharmonicity changes in sign and order of magnitude for both fixed qubit state and variable Φ_{ext} , and variable qubit state and fixed Φ_{ext} .

APPENDIX D: INPUT-OUTPUT THEORY

In Secs. III and IV, we have treated the fluxonium-resonator system as a closed quantum system; experimentally, however, the system is allowed to exchange photons with its waveguide environment. In this appendix, we will attempt to understand quantitatively how the system responds to microwaves traveling through the waveguide.

Depending on its frequency and the relative electric dipole moments of the readout and qubit normal modes, a microwave pulse incident on the fluxonium-resonator system may excite either the readout or qubit mode. We therefore couple transmission lines with impedances Z_R and Z_Q to the readout and qubit modes, respectively, as shown in Fig. 5 [31].

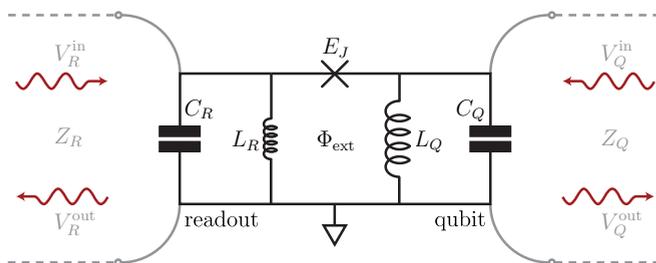


FIG. 5. Electrical circuit schematic for the fluxonium-resonator system (black), showing the decomposition into normal modes coupled by a single nonlinear inductive element. Transmission lines (dashed gray) are weakly coupled (solid gray) to these modes in order to treat the system as a two-port microwave device.

Note that the electrical circuit for the system (solid black in Fig. 5) is drawn according to the Hamiltonian (7) with scaled coordinates [32], so that the intermode coupling is entirely captured by a single nonlinear inductive element. This construction, which considers both transmission lines as the waveguide, allows us to treat dissipation from the system using the two-port microwave scattering matrix approach as opposed to the Lindblad master equation formalism [33].

We proceed by defining the 2×2 impedance matrix Z as that whose elements Z_{ij} are given by

$$V_j = I_i Z_{ij}, \quad (\text{D1})$$

in accordance with Ohm's law, where V_j is the voltage measured across mode j (with R and Q corresponding to readout and qubit, respectively, as in Fig. 5) and I_i is the

current imposed across mode i . In other words, Z_{ij} is the impedance response of the voltage across mode j to a flux across mode i . Taking a time derivative in the Fourier domain, we have

$$Z_{ij} = \chi_{\Phi_i} V_j = i\omega \chi_{\Phi_i} \Phi_j \quad (\text{D2})$$

in the language of linear response theory, where ω is the probe frequency. Employing the spectral expansion of the Kubo formula, we may write

$$Z_{ij} = \sum_{n,\mu} \pi_{n\mu} Z_{ij}^{n\mu}, \quad (\text{D3})$$

where $\pi_{n\mu}$ denotes the population of the state $|n\mu\rangle$ [34,35]. On the other hand, $Z_{ij}^{n\mu}$ represents the impedance response of the system perfectly prepared in the state $|n\mu\rangle$, and it may be expressed as

$$Z_{ij}^{n\mu} = 2i\omega \sum_{n',\mu'} \frac{E_{n'\mu'} - E_{n\mu}}{(E_{n'\mu'} - E_{n\mu})^2 - (\hbar\omega)^2} \times \langle n\mu | \Phi_i | n'\mu' \rangle \langle n'\mu' | \Phi_j | n\mu \rangle. \quad (\text{D4})$$

This expression highlights two crucial facts: the impedance response for the state $|n\mu\rangle$ has poles whenever ω resonates with the $n\mu \rightarrow n'\mu'$ transition and the residues of these poles scale with the matrix elements of the normal mode fluxes between the initial and final transitional states.

The 2×2 scattering matrix S is defined by

$$\begin{pmatrix} V_R^{\text{out}} \\ V_Q^{\text{out}} \end{pmatrix} = S \begin{pmatrix} V_R^{\text{in}} \\ V_Q^{\text{in}} \end{pmatrix}, \quad (\text{D5})$$

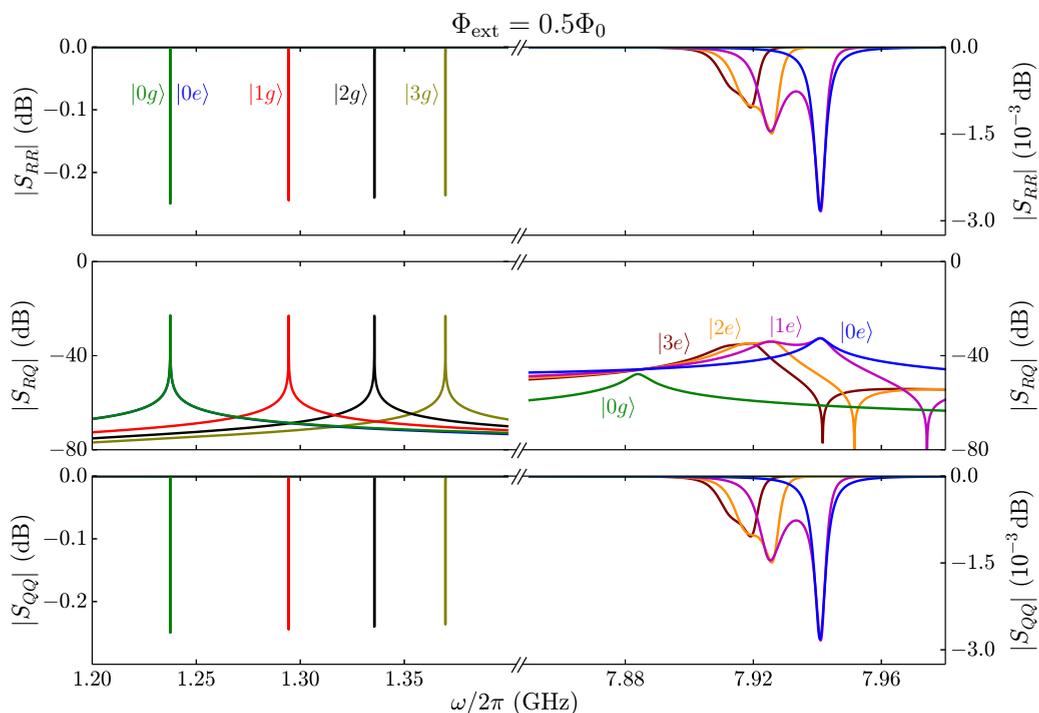


FIG. 6. State-dependent scattering parameter magnitudes for the fluxonium-resonator system at $\Phi_{\text{ext}} = 0.5\Phi_0$. (a) Reflection coefficient amplitude for the readout mode. (b) Transmission coefficient amplitude. (c) Reflection coefficient amplitude for the qubit mode. Amplitudes are plotted at frequencies near the $g \rightarrow e$ qubit transition (left-hand side) as well as those near the $0 \rightarrow 1$ readout transition (right-hand side). Plots are layered from top to bottom in order of ascending energy.

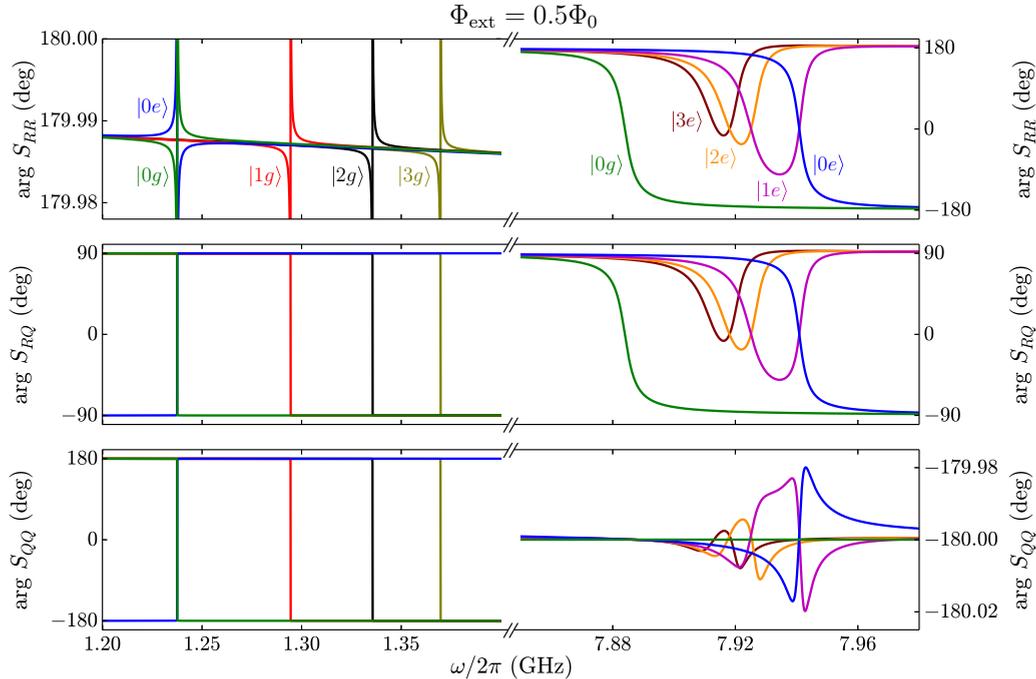


FIG. 7. State-dependent scattering parameter arguments for the fluxonium-resonator system at $\Phi_{\text{ext}} = 0.5\Phi_0$. (a) Reflection coefficient phase for the readout mode. (b) Transmission coefficient phase. (c) Reflection coefficient phase for the qubit mode. Phases are plotted at frequencies near the $g \rightarrow e$ qubit transition (left-hand side) as well as those near the $0 \rightarrow 1$ readout transition (right-hand side). Plots are layered from top to bottom in order of ascending energy.

where V_i^{in} and V_i^{out} depict incoming and outgoing voltage waves for mode i (see Fig. 5). We note that $V_i = V_i^{\text{in}} + V_i^{\text{out}}$ and that the characteristic impedance of the transmission line connected to mode i is defined so that $V_i^{\text{in/out}} = I_i^{\text{in/out}} Z_i$, again invoking Ohm's law. Here, I_i^{in} and I_i^{out} denote incoming and outgoing current waves for mode i , where $I_i = I_i^{\text{in}} - I_i^{\text{out}}$. These relations allow us to write

$$S = (ZZ_0^{-1} + I)^{-1}(ZZ_0^{-1} - I), \quad (\text{D6})$$

where $Z_0 = \begin{pmatrix} Z_R & 0 \\ 0 & Z_Q \end{pmatrix}$ is the characteristic impedance matrix. In our treatment, Z is purely imaginary [see (D4)], and so dissipation via the coupled ports is included by choosing finite characteristic impedances. In particular, we may take $Z_i = Q_i \sqrt{L_i/C_i}$ so that the connected transmission line is matched to the impedance of its normal mode up to multiplication by Q_i , the quality factor of the mode. Choosing $Q_R = 1.5 \times 10^3$ and $Q_Q = 7.5 \times 10^5$, which correspond to a readout resonator linewidth of ~ 5 MHz and qubit relaxation time of $\sim 100 \mu\text{s}$ at $\Phi_{\text{ext}} = 0.5\Phi_0$ for device A, we may calculate the state-dependent scattering parameters plotted in Figs. 6 and 7.

Overall, we see that $|S_{ii}| \approx 1$ (near perfect reflection) and $|S_{RQ}| \approx 0$ (near vanishing transmission), which correspond to our choice of fairly large quality factors and hence weak

coupling to the waveguide. On the other hand, $\arg S_{ii}$ and $\arg S_{RQ}$ experience full 360° and 180° rolls, respectively, at each transition frequency—the exception being that the phase response is very small for S_{ii} near its converse mode transition frequencies, which is due to the weakness of the readout-qubit coupling.

The state-dependent scattering matrix completely characterizes the fluxonium-resonator system in the idealized waveguide environment (as modeled by transmission lines connected to constituent modes). In Figs. 6 and 7, we clearly see readout resonator photon number splitting of the $g \rightarrow e$ qubit transition, a frequency shift of χ in the $|0g\rangle$ and $|0e\rangle$ phase rolls, and a shift in the readout transition frequency depending on the photon number (a manifestation of the self-Kerr effect). We note that more complicated loss mechanisms, such as internal losses, can be added to our model by adding a real part to the impedance matrix. Qualitatively, this will draw the reflection coefficient magnitudes away from unity toward zero (in the limit of critical coupling).

We note that the experimental setup used for the measurements in Sec. IV does not allow for complete access to the photons leaking out of the qubit mode. However, in fluorescence experiments that intentionally couple the microwave environment to the qubit, we expect these state-dependent scattering parameters to agree well with measurements.

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